

TA-1144





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SECTION 1 TECHNICAL DESCRIPTION

1-1. TECHNICAL SPECIFICATIONS

Technical specifications for the TA-1144 are listed in Table 1-1.

TABLE 1-1. TA-1144 TECHNICAL **SPECIFICATIONS**

Power Amplifier Section

Dynamic power:

70 watts, both channels

operating

Rated output:

30 watts per channel, both

channels operating

Power bandwidth:

10 Hz to 50 kHz, IHF

(15 watts per channel)

20 Hz to 20 kHz

(30 watts per channel)

Harmonic distortion:

Less than 0.1% at 1 kHz rated

output

IM distortion:

Less than 0.2% at rated

output

Input impedance:

 $100\,k\Omega$

Input sensitivity:

0.8V

(for rated output)

Signal-to-noise ratio: greater than 90 dB

(shorted input)

Preamplifier Section

Frequency response:

PHONO-1, -2,

RIAA curve ±0.5 dB

TAPE, TUNER,

AUX-1, -2, -3, 10Hz to 100kHz ±9 dB

Input sensitivity

and impedance:

PHONO-1, -2

1.2 mV 47 k

AUX-1, -2, -3 TUNER,

TAPE × REC/PB

(x General Export Model only)

150 mV 100 k

Signal output and

output impedance:

REC OUT 150 mV 10 k

PRE OUT 900 mV 15 k

※ REC/PB 20 mV 80 k

(x General Export Model only)

Signal-to-noise ratio: PHONO-1, -2

greater than 70 dB

(weighting network "B")

AUX-1, -2, -3 TUNER,

TAPE

(General Export Model only)

greater than 90 dB

(weighting network "A")

Tone controls:

BASS ±10 dB at 100 Hz

(2 dB/step)

TREBLE ±10 dB at 10 kHz

(2 dB/step)

Filters:

HIGH -6 dB/oct

above 5 kHz LOW -6 dB/oct

below 100 Hz

Loudness control:

50 Hz, +8dB 10kHz, +4dB

(at -30 dB attenuation

setting)

Power consumption: Approx. 132W

(USA, CANADA Model)

Approx. 177W

(General Export Model)

Power requirement:

117V ac

(USA, CANADA Model only) 100, 117, 220, 240V ac

(General Export Model only)

Dimensions:

422 mm (width) x 148 mm

(height) × 321 mm (depth) 16^{5} /8" (width) × 5^{13} /16"

(height) $\times 12^{5/8}$ " (depth)

Net weight:

7.8 kg (17 lb 1 oz)

Shipping weight:

12.3 kg (26 lb 15 oz)

1-2. DETAILED CIRCUIT ANALYSIS

The following describes the functions or operations of all stages and controls. The text sequence follows signal paths. Stages are listed by transistor reference designation at the left margin; major components are also listed in a similar manner.

Since the audio-amplifier section contains two identical amplifier chains, only the left channel will be described. Refer to the block diagram on page 8 and schematic diagram on pages 27 to 28.

Stage/Control

Function

Preamplifier Section

Equalizer amplifier Q101, Q102 This direct-coupled two stage amplifier amplifies the small signal provided by the phono cartridge (and applied to PHONO-1 and PHONO-2 input terminal) to the level required at the input of the following tone-control circuit.

Bias circuit R107, R102, R103

Dc bias voltage for Q101 is extracted from R107 in the emitter circuit of Q102 and fed back to the base of Q101 through R102 and R103. This dc negative feedback technique provides stable operation

Equalization circuit R105

RIAA equalization is achieved by the negative-feedback loop R110, R111, R112 containing R110, R111, R112, R105, C105 and C106.

during temperature changes.

C105, C106

Be sure to use replacement components with the exact same values.

R114 (R214) in the output prevents interaction between left and right channelequalization when the MODE switch is set to L+R.

MODE switch **S4**

In the STEREO position of S4, left and right input signals are routed to their respective amplifiers. In the L+R position, the left and right signals are added and the sum is then fed to both amplifier channels. A rotary switch having two sections is used to obtain L+R signal even if the MONITOR switch is set to the TAPE position.

Stage/Control

Function

VOLUME control R125

The equalized phono signals and signals applied to the other input terminals are fed to the VOLUME control through the MONITOR and MODE switches. The level of the signal applied to the following tone control circuit is determined by the setting of R125.

R124

BALANCE control Employed to optimize stereo reproduction. To eliminate insertion loss at the mechanical center of movement, a special potentiometer having a conductive coating over half its element length is used.

LOUDNESS switch **S**5

This switch and R126, R127 C121 and C122 compensate for the characteristics of the human ear which vary according to the loudness of the sound being heard. When this switch is set to ON and the VOLUME control is set for 30 dB attenuation, the overall frequency response is increased 8 dB at 50 Hz and 4 dB at 10 kHz in relation to the level at 1 kHz.

Tone-control amplifier Q103, Q104 This direct-coupled two-stage amplifier has basically flat response, but it operates as a negafive-feedback type tonecontrol circuit. The output generated at the collector circuit of Q104 is fed back to the emitter circuit of Q103 through the treble and bass tone-control network.

TREBLE control S6, (S7) R151 to R160 (R251 to R260)

Increases or decreases the amount of negative feedback voltage by switching the filter resistors in steps. Each switch step changes the treble response approximately 2 dB at 10 kHz.

BASS control S8, (S9) R161 to R170 (R261 to R270) Similar to the treble control except for filter components and frequency characteristics. this circuit, negative feedback and conventional RC network (R144, C140) techniques are applied to obtain proper attenu-

Stage/Control	Function	Stage/Control	Function
BASS control	ation at low frequencies. Each step of this switch changes the bass response approximately 2 dB at 100 Hz.	Ac balance adj.	Q301's emitter is connected to the negative power supply through R306 and R307 (ac balance adj.). To obtain the minimum
LOW FILTER switch S10	The high-pass filter (C141 and R145) cuts out unwanted low frequency components (100 Hz and lower) from the input signal when this switch is ON. These unwanted low frequencies include rumble created by the turntable record changer, or the record itself.	Predriver Q302	harmonic distortion, R307 is adjusted to set the output terminal at zero volt dc. Though this stage is a conventional flat amplifier, it determines the output voltage swings because the following stages are basically in the emitter-follower
HIGH FILTER S11	Eliminates unwanted high-frequency components (5 kHz and higher) from the input signal when ON.		configuration. The ac load resistor for this stage is R313. C304 forms a bypass circuit around Q303 to drive Q304 effectively.
PRE*AMP/POWER AMP switch S12	In NORMAL, the output of the tone control circuit is fed to the power amplifier's input through S12. In SEPARATE, the output of the tone control circuit is disconnected from the power amplifier's input terminal, allowing you to use the sections separately.	Dc bias adj. (idling current) Q303, R310	Q303 is forced to conduct and operates as a small resistance providing the necessary forward bias on the two cascaded emitter-followers. R310 controls the base bias of Q303, determining the impedance between the emitter and collector of Q303, and thereby controls the dc bias
Preamplifier Q301	Amplifies the input signal to the level required for the following driver stage. The ac output appears across load resistor R308 (2.2 k) in the collector circuit. Emitter decoupling capacitor C302 and resistor R305 in the emitter circuit form a frequency-selective ac bypass circuit to reduce the amplifier's gain at very low frequencies.	Thermal compensator for dc bias D302	voltage for the following complementary circuit. The negative temperature coefficient of D302 provides thermal compensation for the complementary and power transistor circuits. D302 is attached to the power transistor's heat sink to detect heat increases in the power transistors.
Thermal compensation D301, D501	As all the stages are directly coupled, dc stability is required. The negative temperature coefficient of D501 provides thermal compensation for this stage, and D301 compensates the following driver stage's operation. To obtain sufficient stability, dc negative feedback via R326, R306 and R307, and ac negative feedback via R326, R305, C307 and C302 are provided.	Driver Q304, Q305 (Complementary circuit)	These transistors operate as emitter-followers to provide the current swings demanded of the output stages and also proivde the necessary phase inversion. Phase inversion is performed by using PNP and NPN type transistors. Resistors R318 and R315 in the collector circuit limit the maximum current flow (which occurs when the output is

Stage/Control

Function shorted to protect the tran-

sistors from destruction.

Stage/Control

Function

Power transistor Q306, Q307

The output transistors (Q306 and Q307) are connected directly to a power supply of about ±40V potential. Q306 supplies power to the load during the positive half cycle and Q307 operates during the negative half cycle. As a result, the large coupling capacitor at the output (which may cause power loss or distortion at low frequencies) is eliminated.

R321, R322

R321 and R322 (0.5Ω) are inserted in the output circuit of the power transistors to avoid nonlinear distortion and improve stability.

Heat-sensitive overload protection circuit Q503, Q504 To protect overloaded power transistors from destruction, a heat-sensitive protection circuit is employed.

It operates as follows:

Under normal conditions, voltdividers consisting of resistors and posistors (resistors having a positive temperature coefficient) are arranged to place nearly zero bias on Q504, thereby cutting it off. Though the collector of Q504 is directly coupled to the base of Q502 (ripple filter), it has no effect upon Q502's operation. The same is true of Q503, which is connected to the base of Q501 (ripple filter) except for its bias circuit. The base of Q503 is connected to the positive and negative ripple filter output through R513 (10k) and R512 (10 k) respectively. This places nearly zero bias upon O501. and cuts it off.

In the event of a short circuit at the output terminals or a thermal runaway, excessive current flows in the power transistors (for the amount of drive voltage supplied), causing the power transistors to overheat.

The heat caused by excessive dissipation at the collectors of the power transistors is sensed by the posistor attached to the transistors. These posistors have a positive temperature coefficient so the heat causes their resistance to increase at some specified temperature.

This places forward bias voltage on Q504. The two posistors are arranged as an OR gate, so a malfunction in either channel will be detected. Q504's turnon turns off Q502, thereby reducing the negative supply voltage. This also makes the positive supply voltage decrease because the reduction of negative supply voltage increases the positive bias voltage upon Q503, forcing it into conduction. As a result, Q501 turns off, cutting off all power to the driver stages.

Now the driver stages cannot drive the power transistors despite an input signal. Since the output transistors are operated close to class B, the absence of drive reduces their collector current to practically zero.

Power Supply Rectifier D504 A full-wave bridge rectifier provides a positive and a negative dc power supply for the power amplifier.

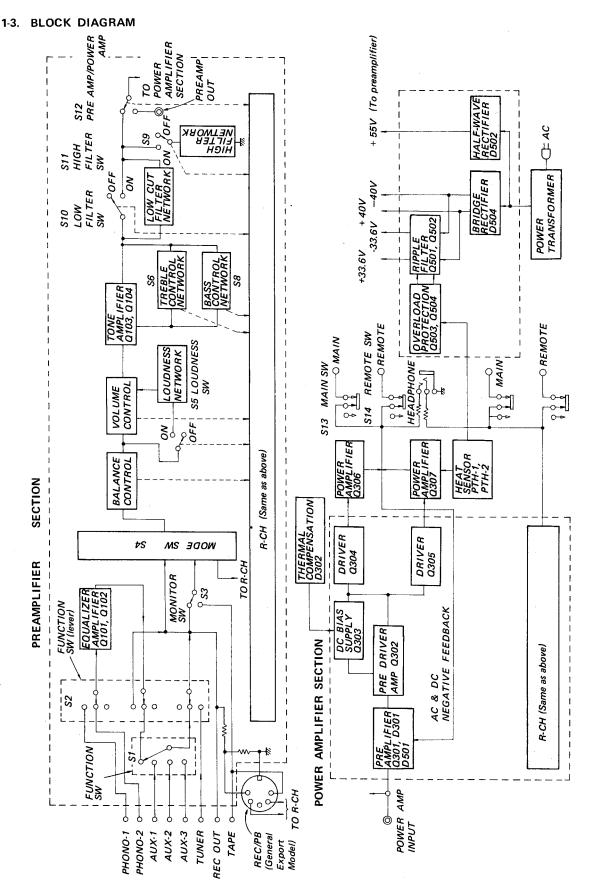
Rectifier D502 A half-wave rectifier (D502) and ripple filter (C513, R510, C505) supply well-filtered dc power to the preamplifier section of the TA-1144.

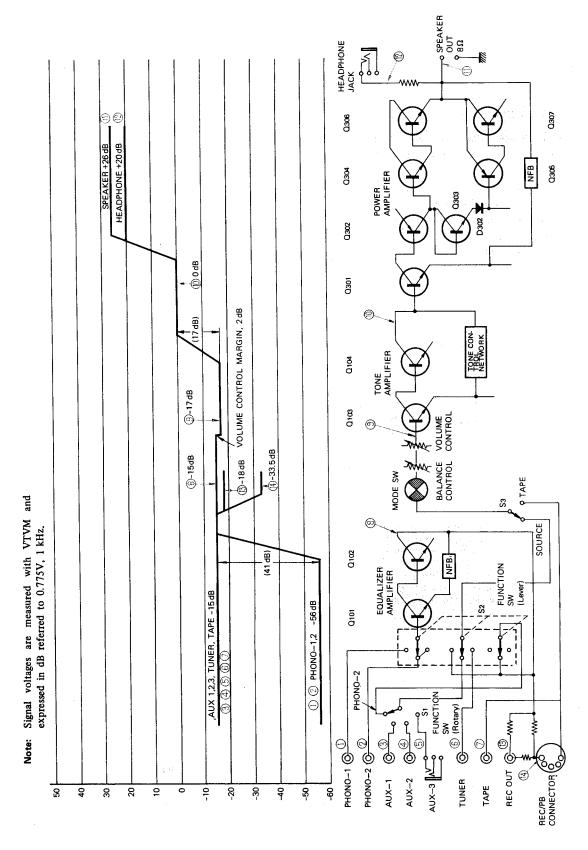
Ripple filter Q501, Q502 R506, R507 C515, C516, C517, C518 These components reduce the ripple voltages in the dc power supply for the preamplifier and predriver stages of the power amplifier section to an extremely-low value.

Q501 and Q502 serve as an electronic filter to supply well filtered dc of about ±33.6V to

Stage/Control	Function	Stage/Control	Function
	each stage. The ripple filters also serve as a muting circuit and are part of the overload protection circuit.		emitter circuit of Q301 is relatively small. R506 and C516 (R507 and C515) comprise an RC network with a long time constant. This eliminates pop- ping because Q501 and Q502
Muting circuit	"Popping" noise due to initial charging current flow to the electrolytic capacitor in the		are brought into conduction gradually when the POWER switch is turned on.

TA-1144





SECTION 2

DISASSEMBLY AND REPLACEMENT PROCEDURES

WARNING

Unplug the ac power cord before starting any disassembly or replacement procedures.

2-1. TOOLS REQUIRED

The following tools are required to perform disassembly and replacement procedures on the TA-1144.

Screwdriver, Phillips-head
Electric drill and bits
Screwdriver, 3 mm (½") blade
Tape, electrical
Wrench, adjustable
Diagonal cutters
Pliers, long-nose
Pliers, gripping
Soldering iron, 40 to 150W
Silicone grease
Solder, rosin core
Prick punch
Cement solvent

2-2. HARDWARE IDENTIFICATION GUIDE

The following chart will help you to decipher the hardware codes given in this service manual.

Note: All screws in the TA-1144 are manufactured to the specifications of international Organization for Standardization (ISO). This means that the new and old screws are not interchangeable because ISO screws have a different number of threads per mm compared to the old ones. The ISO screws have an identification mark on their heads as shown in Fig. 2-1.

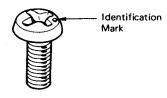
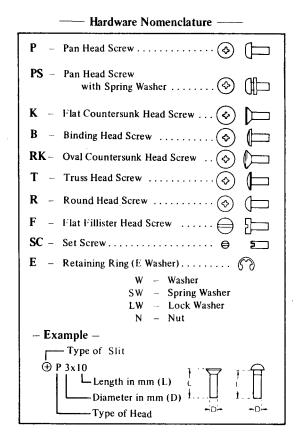


Fig. 2-1 ISO screw



2-3. TOP COVER REMOVAL

Remove the two machine screws at each side of the amplifier, and lift off the top cover.

2-4. FRONT PANEL REMOVAL

- Remove the top cover as described in Procedure 2-3.
- Remove the all control knobs by simply pulling them off.
- 3. Remove the three ornamental rings by loosening the hex-nuts securing them to the front panel as shown in Fig. 2-2.
- 4. Remove the three screws (⊕PS 4×6) behind the top edge of the front subchassis assembly, as shown in Fig. 2-3.
- 5. Remove the two screws (@P3x6) from the front bottom edge of the amplifier securing the front panel to the front subchassis, as shown in Fig. 2-4. This frees the front panel.

2-5. REAR PANEL REMOVAL

- 1. Remove the top cover as described in Procedure 2-3.
- 2. Remove the four self-tapping screws (\oplus P 3×6) securing the rear panel to the bottom plate, as shown in Fig. 2-4. This frees the rear panel.

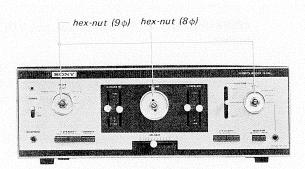


Fig. 2-2 Hex-nut removal

2-6. PILOT LAMP REPLACEMENT

- Remove the top cover as described in Procedure 2-3.
- 2. Straighten the tab of the pilot-lamp holder to permit the removal of the lamp socket; then pull out the lamp socket. See Fig. 2-3.
- 3. Unscrew the lamp and remove the plastic tube and then install the replacement lamp.

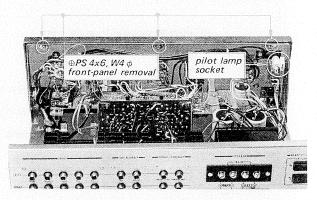


Fig. 2-3 Front-panel removel (1)

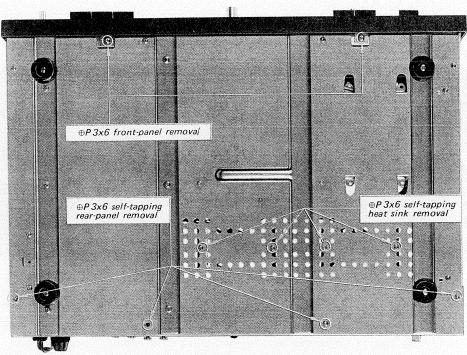


Fig. 2-4 Bottom view

2-7. CONTROL AND SWITCH REPLACEMENT

Note: The SPEAKER and LOUDNESS switches are mounted on one circuit board. The same is true for the FILTER and MONITOR switches, and for each TONE control. When replacing any of the abovementioned controls or switches, replace the whole circuit board for quick service. See boards listed below.

SERVICE SPARE PARTS LIST

Part No.	Description
98-2555-01	FILTER/MONITOR switch board
98-2555-02	SPEAKER/LOUDNESS switch board
98-2555-03	TONE (TREBLE) control board
98-2555-04	TONE (BASS) control board

Preparation

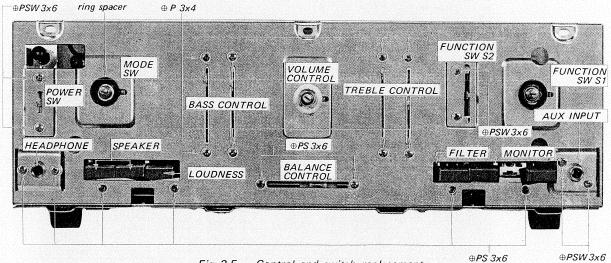
Remove the front panel as described in Procedure 2-4.

POWER Switch, FUNCTION Lever and TONE Controls

- 1. Remove the screws ($\oplus PSW3\times6$) securing the switch or control to the front subchassis as shown in Fig. 2-5.
- 2. Unsolder the leads or components from the switch or control lugs, then solder them to a new one.
- 3. Install the new switch or control.

MODE or Rotary FUNCTION Switch, and VOLUME control

- 1. Apply a drop of cement solvent to the plastic ring spacer and wait a few seconds for the cement to dissolve, then pry out the spacer with a screw driver.
- Remove the hex nut securing the switch or control to the front subchassis.
- 3. Unsolder the lead wires from the switch or control lugs one by one. Solder them to a new switch, then install it.



SPEAKER/LOUDNESS and FILTER/MONITOR switch boards

- 1. Pull off the push buttons. If necessary, cover the buttons with tape and use pliers to pull them off. Take care not to scratch the buttons.
- 2. Remove the two screws (⊕PS3×6) securing the printed circuit board to the front subchassis. See Fig. 2-5.
- 3. Remove the self-tapping screw ($\oplus P 3\times 6$) securing electrolytic capacitor C505 (Fig. 2-6) to the bottom plate, if necessary, then remove the capacitor.
- Unsolder the lead wires from the printed circuit board and solder them to the new one.
- 5. Remove the defective switch board and install the replacement.

BALANCE Control

- 1. Remove the preamplifier board by loosening the four screws (⊕PS 3×6) securing it to its mounting bracket. See Fig. 2-6.
- 2. Remove the two screws (@PS 3x6) securing

- the control to the front subchassis as shown in Fig. 2-5.
- 3. Unsolder the leads from the control, then solder them to a new one.
- 4. Install the replacement BALANCE control.

2-8. POWER TRANSISTOR REPLACEMENT

- Remove the top cover as described in Procedure 2-3.
- 2. Remove the two self-tapping screws (\oplus P 3×6) securing the heat sink to the bottom plate as shown in Fig. 2-4.
- 3. Cut the emitter and base leads of the defective power transistor with a diagonal cutter.
- Remove the two screws (⊕P3×12) and nuts securing the power transistor to the heat sink, then install a new transistor. See Fig. 2-7.
- 5. When replacing the power transistor, apply a coating of silicone grease to both sides of the insulating mica washer.

Any excess grease, squeezed out when the mounting bolts are tightened, should be wiped off with a clean cloth. This prevents the grease from accumulating conductive dust particles that might eventually cause a short.

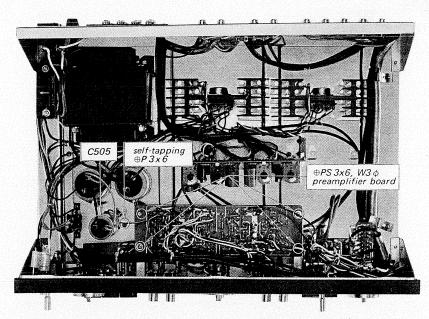


Fig. 2-6 C505 removal and preamplifier removal



2-9. REPLACEMENT OF COMPONENTS SECURED TO THE REAR PANEL BY RIVETS

- 1. Remove the rear panel as described in Procedure 2-5.
- Bore out the rivet using a drill bit slightly larger in diameter than the rivet as shown in Fig. 2-8.

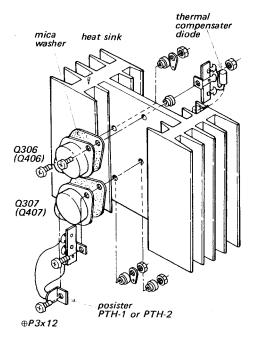


Fig. 2-7 Power transistor replacement

- 3. When the peened end is bored away, punch out the remainder of the rivet with a nail set or prick punch.
- 4. Remove the defective component, and then install a new one.
- 5. Secure the new component with a suitable screw and nut or a repair rivet screw (part number 3-701-402).

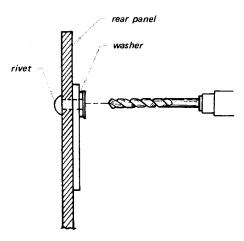
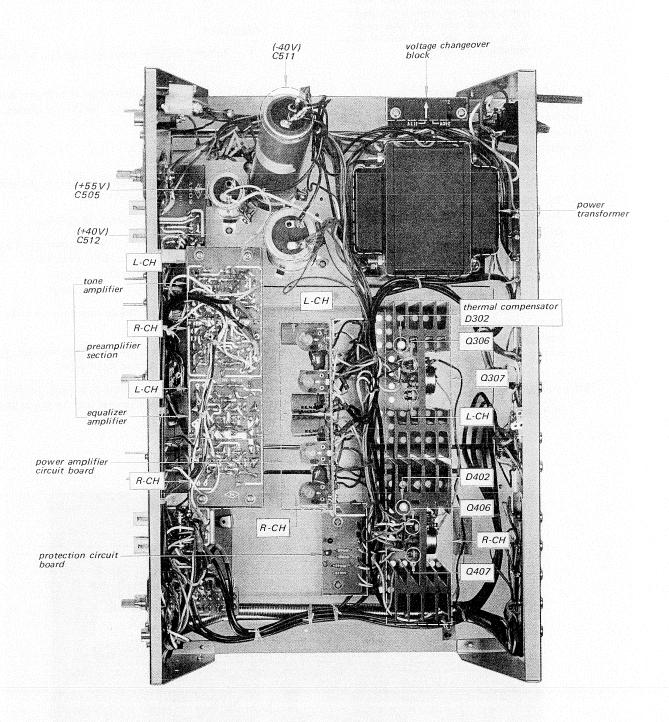


Fig. 2-8 Rivet replacement

2-10. CHASSIS LAYOUT





SECTION 3 ADJUSTMENT

Note: There are two adjustments in the power amplifier, a dc-bias adjustment and an ac-balance adjustment. These adjustments should be alternately repeated two or three times after replacing any of the power transistors until the best operation is obtained.

3-1. DC BIAS ADJUSTMENT

Serious deficiencies in performance, such as thermal runaway of power transistors, will result if this adjustment is improperly set.

CAUTION

To avoid accidental power transistor damage, increase the ac line voltage gradually (using a variable transformer) while measuring the voltage across emitter resistors R321 and R322 (or R421 and R422) as shown in Fig. 3-1. Check to see that the reading does not exceed 50 mV. If it does, turn off the power immediately, then check and repair the trouble in the power-amplifier board.

Test Equipment Required

1. Dc millivoltmeter

- 2. Variable transformer
- 3. Screwdriver with 3 mm (1/8") blade

Preparation

- Remove the top cover as described in Procedure 2-3.
- 2. Connect the dc millivoltmeter between R321 and R322 (R421 and R422) as shown in Fig. 3-1.

Procedure

- 1. Apply a drop of cement solvent to the semi-fixed resistors (Fig. 3-1).
- Set the semifixed resistors as follows:
 R310 (L-CH, dc bias)..... fully counterclockwise
 R410 (R-CH, dc bias).... fully clockwise
 R307, R407 (ac balance)

..... midposition

- 2. Set the variable transformer for minimum output.
- 3. Turn the POWER switch, then increase the line voltage up to the rated value.
- 4. Apply a drop of cement solvent to R310 (R410) then wait a few seconds for the cement to dissolve.

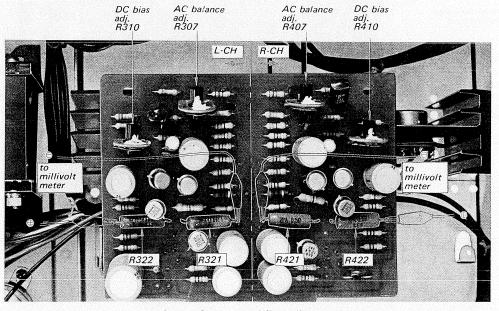


Fig. 3-1 Power amplifier adjustment

5. Adjust R310 (R410) to obtain a $50\,\mathrm{mV}$ reading on the meter.

3-2. AC BALANCE ADJUSTMENT

Excessive harmonic distortion at high levels will result if this adjustment is improperly set.

Test Equipment Required

- 1. Dc null meter or dc millivoltmeter
- 2. Screwdriver, with 3 mm (1/8") blade

Preparation

- Remove the top cover as described in Procedure 2-3.
- 2. Set the SPEAKER switch to MAIN.

3. Connect the dc null meter or dc millivoltmeter to the MAIN speaker output terminal.

Procedure

- 1. Apply a drop of cement solvent to R307 (R407) and wait a few seconds for the lock paint to dissolve.
- 2. Turn the POWER switch to ON, and then adjust R307 (R407) to obtain a OV reading on the meter.
- After 10 minutes warm-up, alternately repeat this and the dc bias adjustment two or three times.
- 4. After completing the adjustment, apply a drop of lock paint to R310 and R307 (R410 and R407).

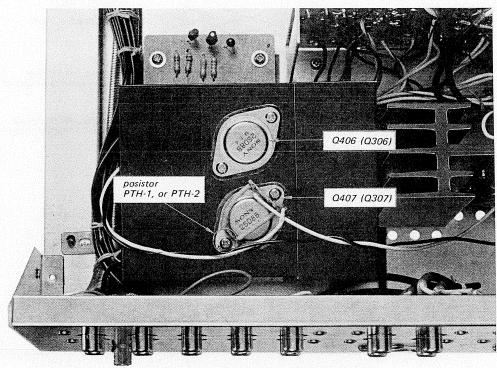


Fig. 3-2 Parts location



SECTION 4 REPACKING

The TA-1144's original shipping carton and packing material is the ideal container for shipping the unit. However, to secure the maximum protec-

tion the TA-1144 must be repacked in this material precisely as before. The proper repacking procedure is shown in Fig. 4-1.

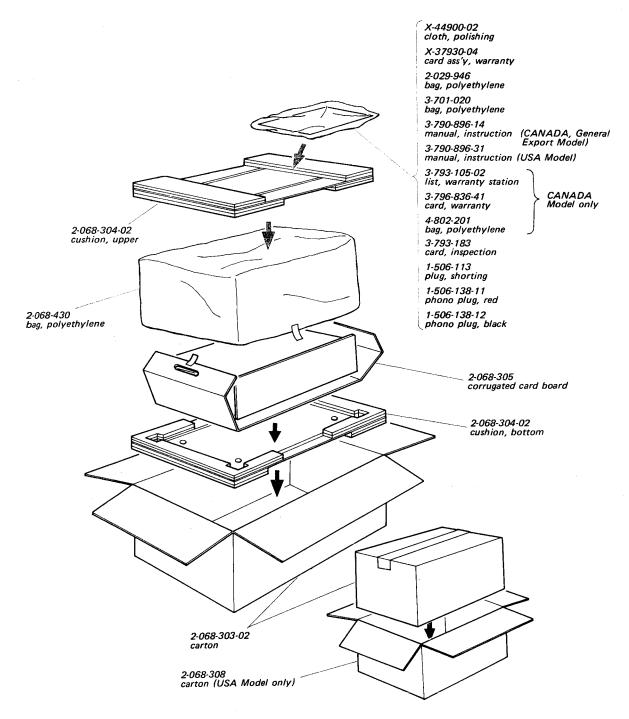
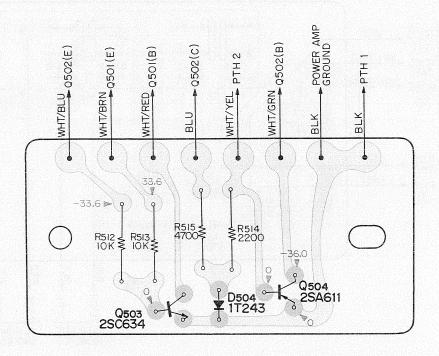


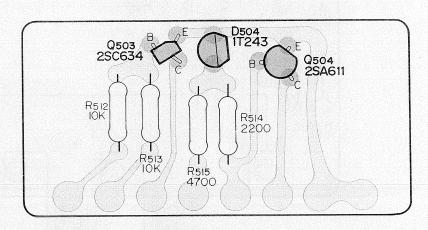
Fig. 4-1 Repacking

SECTION 5 DIAGRAMS

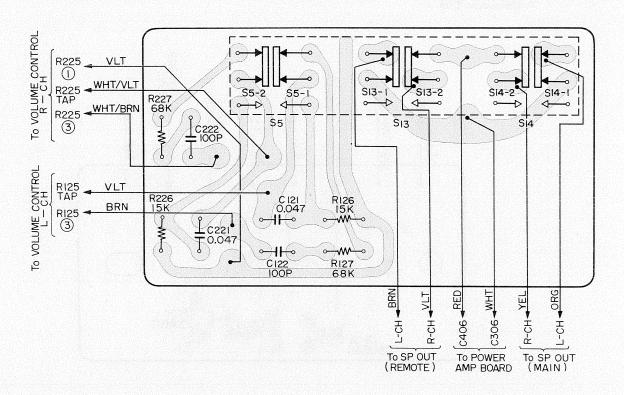
5-1. MOUNTING DIAGRAM — Protection Circuit Board — — Conductor Side —



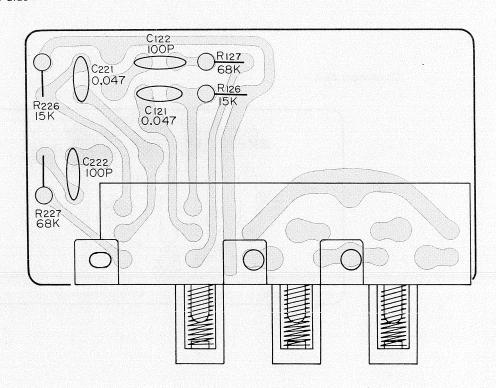
- Component Side -



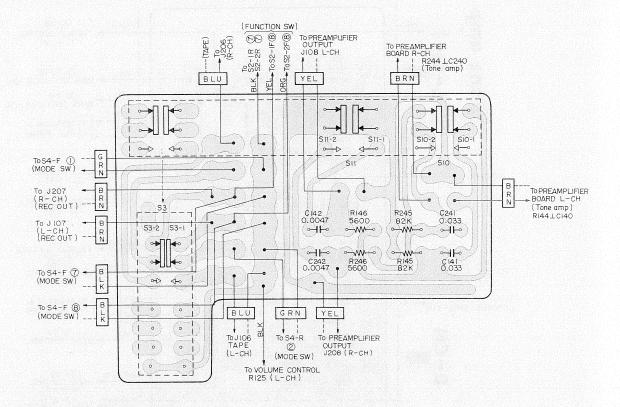
5-2. MOUNTING DIAGRAM - Speaker, Loudness Switch Board - - Conductor Side -



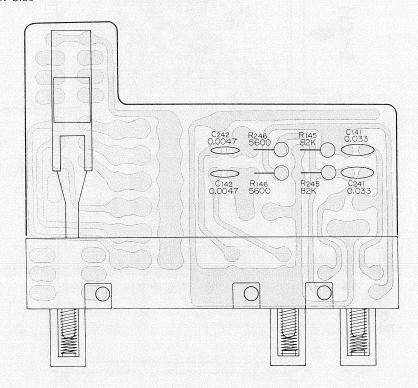
- Component Side -



5-3. MOUNTING DIAGRAM — Filter, Monitor Switch Board — — Conductor Side —

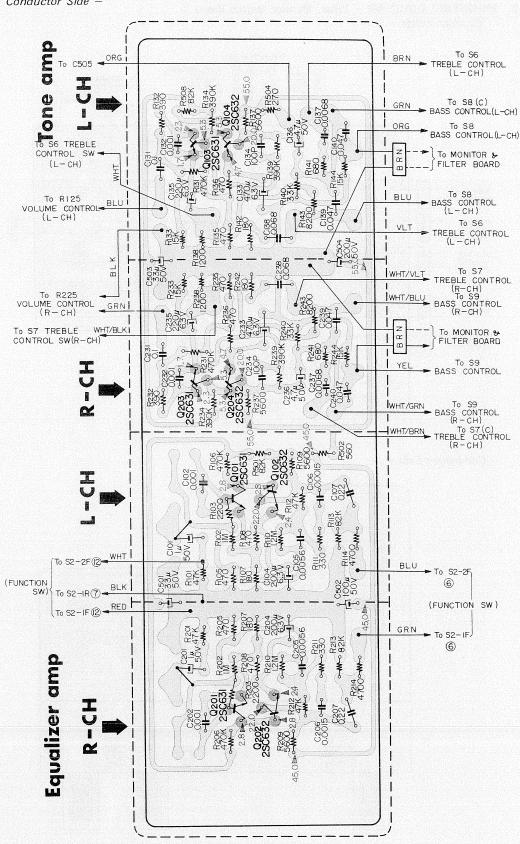


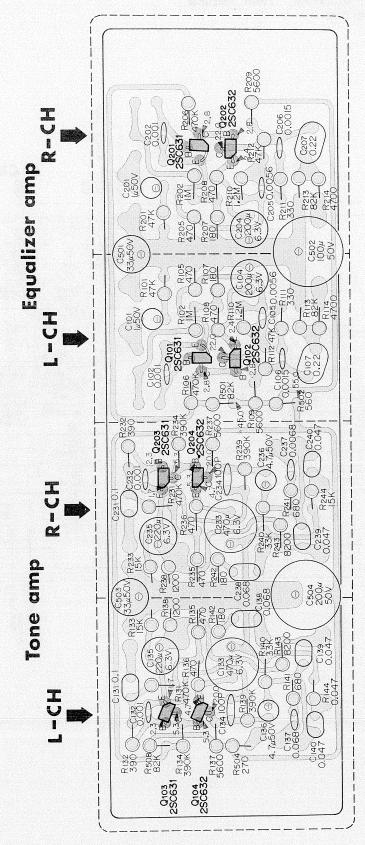
- Component Side -



5-4. MOUNTING DIAGRAM - Preamplifier Section -

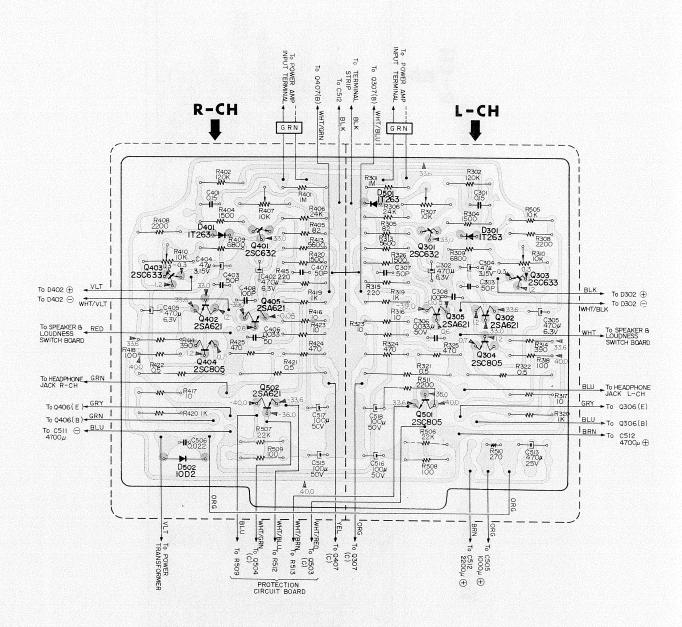
- Conductor Side -

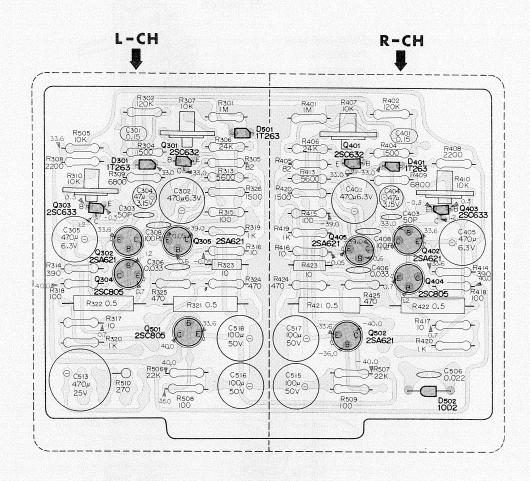






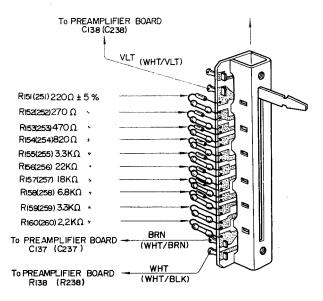
5-5. MOUNTING DIAGRAM — Power Amplifier — — Conductor Side —





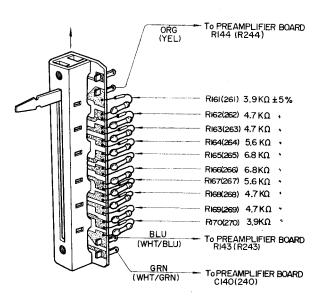
5-6. MOUNTING DIAGRAM - Tone Control Switch -

- Treble Control -



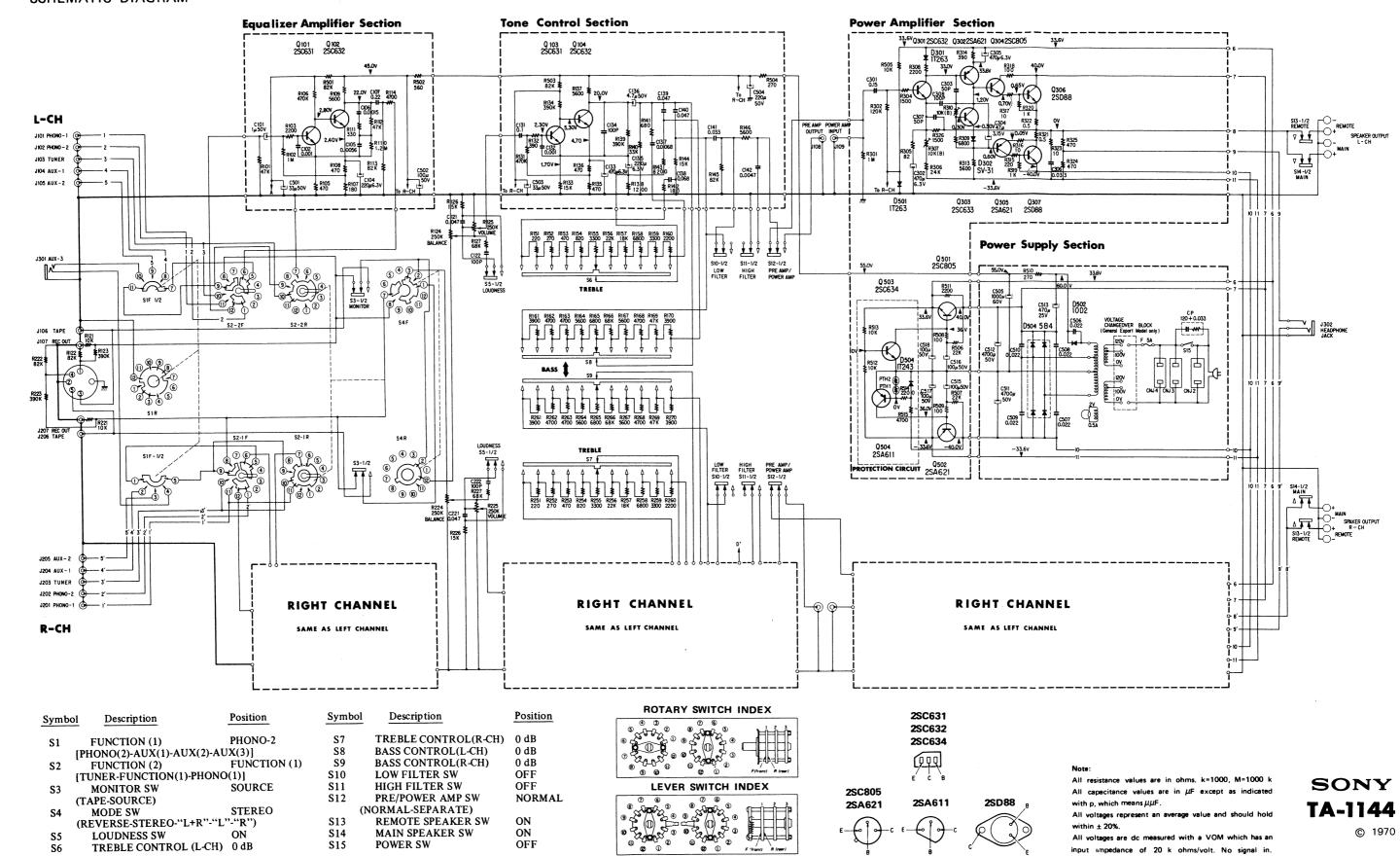
()INDICATES RIGHT CHANNEL

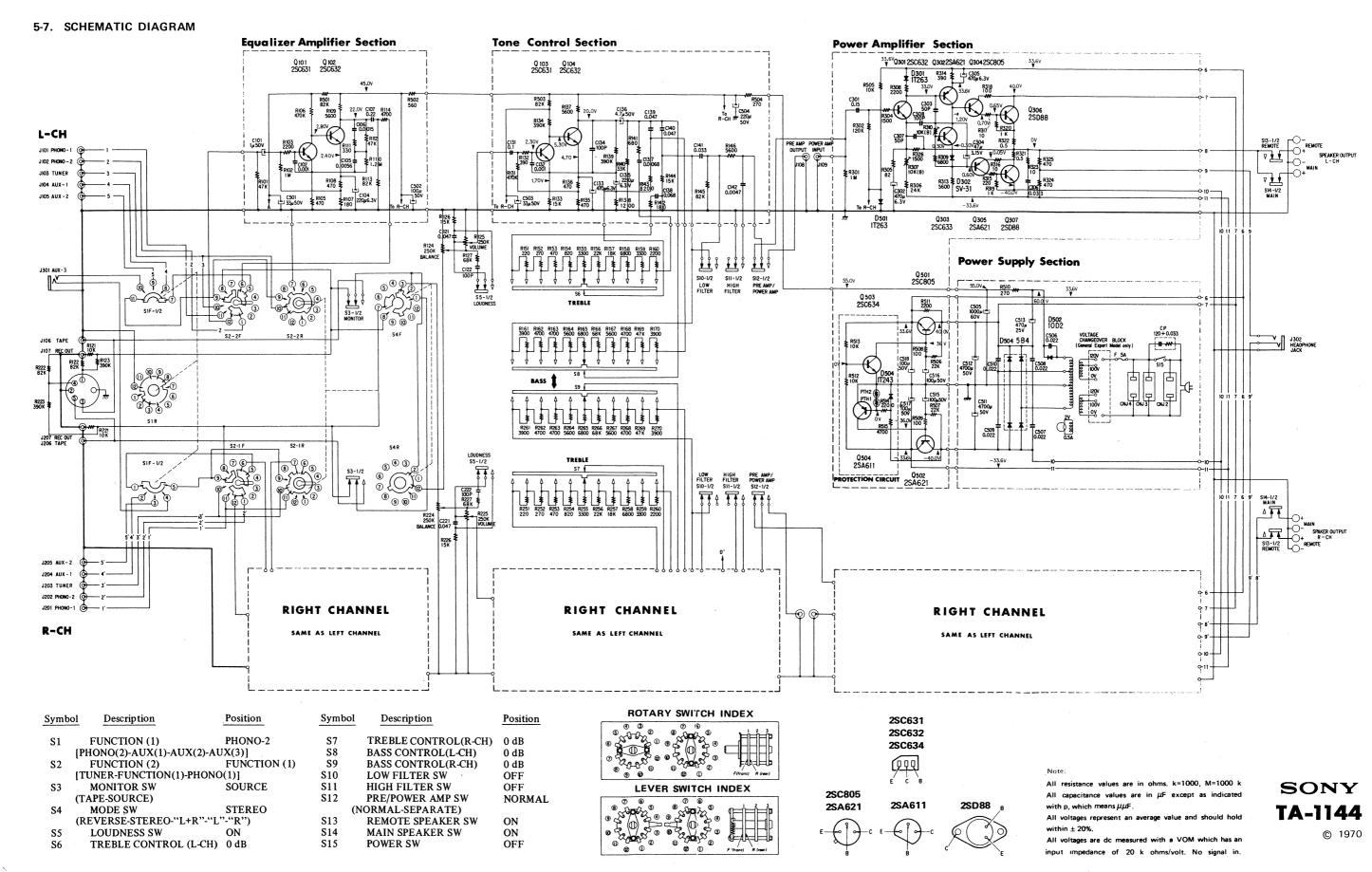
- Bass Control -



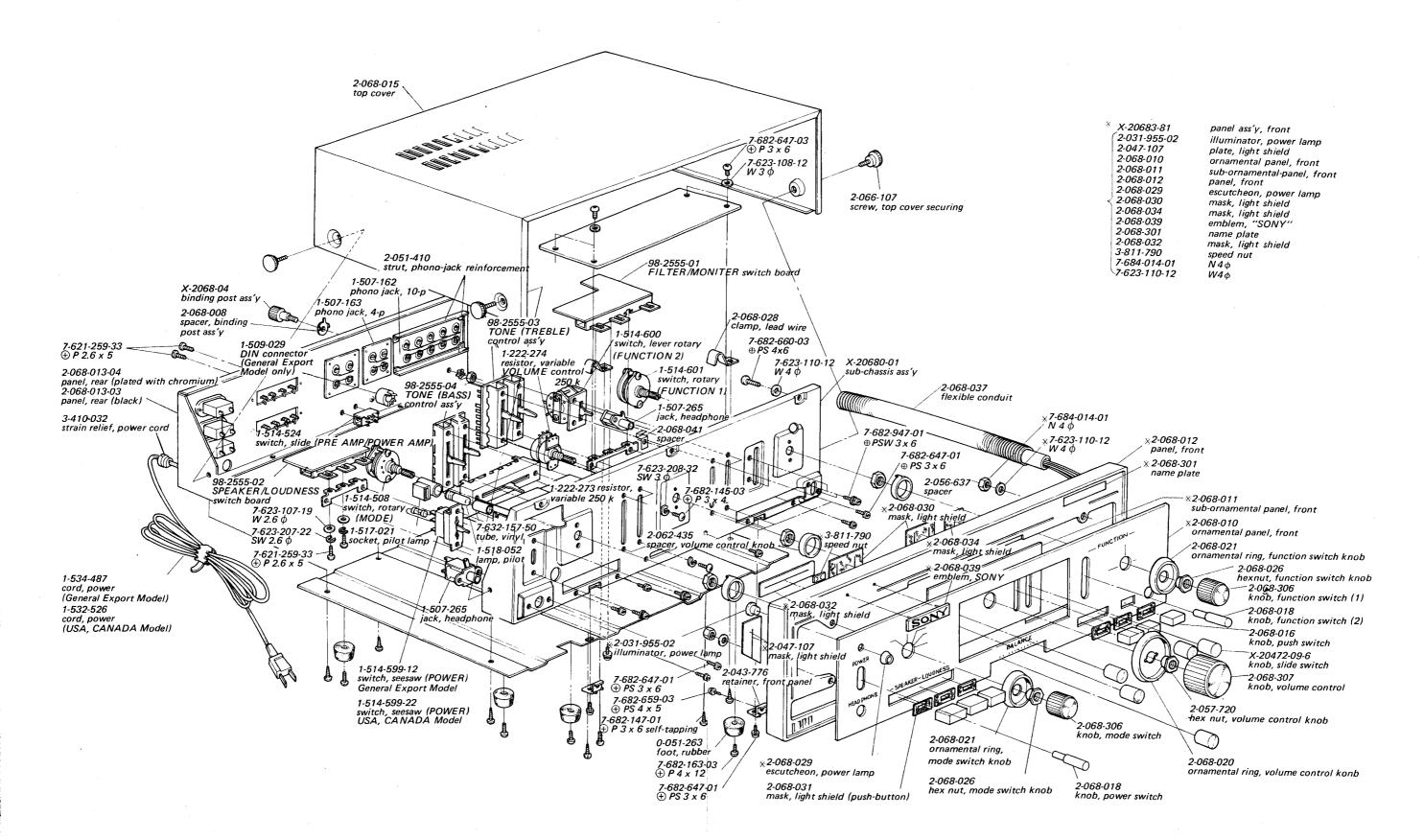
()INDICATES RIGHT CHANNEL

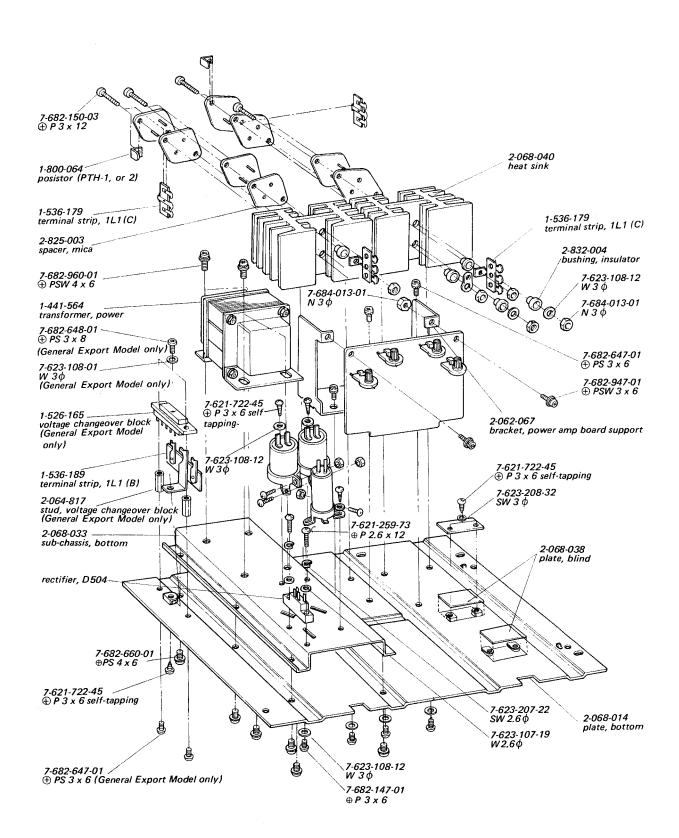
SCHEMATIC DIAGRAM





SECTION 6 EXPLODED VIEW







SECTION 7 ELECTRICAL PARTS LIST

Ref. No.	Part No.	Descr	ription	Ref. No.	Part No.	I	Descriptio	n	
			<u>- P</u>	103.110.	147770.	Description			
	MOUNTED C	IRCUIT BOAI	RDS	C104(C204)	1-121-295	220	$\pm^{100}_{10}\%$	6.3V,	electrolytic
	98-2555-01	FILTER/MO	ONITOR switch board	1	1-105-510-12	0.0056	±5%	50V,	mylar
	98-2555-02		LOUDNESS switch board	1 '	1-105-503-12	0.0015	±5%	50V,	mylar
	98-2555-03	,	EBLE) control ass'y	1	1-105-689-12	0.22	±10%	50V,	mylar
	98-2555-04	TONE (BAS	S) control ass'y		1-105-681-12	0.047	±10%	50V,	mylar
	98-2555-21		r circuit board	C122(C222)	1-107-004	100 p	±10%	500V,	silvered mica
	98-2555-22	power ampl	ifier circuit board	1	1-105-685-12	0.1	±10%	50V,	mylar
	X-20680-27	protection of	circuit board	C132(C232)	1-105-821-12	0.001	±20%	50V,	mylar
				C133(C233)	1-121-359	470	$\pm^{100}_{10}\%$	6.3V,	electrolytic
				C134(C234)		100p	±10%		silvered mica
				C135(C235)	1-121-295	220	$\pm^{100}_{10}\%$	6.3V,	electrolytic
		NDUCTORS		C136(C236)	1-121-346	4.7	$\pm^{100}_{10}\%$	50V,	electroly tic
D301(D401	1)	diode	1T263	C137(C237)	1-105-671-12	0.0068	±10%	50V,	mylar
D302(D402	2)	diode	SV31	C138(C238)	1-105-683-12	0.068	±10%	50V,	mylar
D501		diode	1T263	C139(C239)	1-105-681-12	0.047	±10%	50V,	mylar
D502		diode	10D2	C140(C240)	1-105-681-12	0.047	±10%	50V,	mylar
D503		diode	5B4	C141(C241)	1-105-679-12	0.033	±10%	50V,	mylar
D504		diode	1T243M	C142(C242)	1-105-669-12	0.0047	±10%	50V,	mylar
Q101(Q201)	transistor	2SC631	C201(C401)	1 105 (07 12	0.15	±1.0 <i>c</i> c	50¥7	•
Q101(Q201		transistor	2SC632	C301(C401)	1-105-687-12	0.15	±10%		mylar
Q103(Q203		transistor	2SC631	C302(C402)		470			electrolytic
Q104(Q204		transistor	2SC632	C304(C404)		50 p	±10%		silvered mica
Q (Q. 2		tiuiisistoi	250032	C305(C405)		47 470			electrolytic
Q301(Q401)	transistor	2SC632		1-121-339	0.033	±10%		electrolytic
Q302(Q402		transistor	2SA621	C307(C407)		50p	±10%		mylar silvered mica
Q303(Q403	-	transistor	2SC633	C308(C408)		100p	±10%		silvered mica
Q304(Q404	•	transistor	2SC 805	C300(C400)	1 107 004	100р	±10 <i>70</i>	JUV,	silvered filica
Q305(Q405		transistor	2SA621	C501	1-121-351	33	±100%	50V	electrolytic
Q306(Q406	5)	transistor	2SD88	C502	1-121-384	100	±100%		electrolytic
Q307(Q407	"	transistor	2SD 88	C503	1-121-351	33	±100%		electrolytic
				C504	1-121-385	220	±100%		electrolytic
Q501		transistor	2SC805	C505	1-121-330	1,000	- 10,0		electrolytic
Q502		transistor	2SA621	C506	1-105-877-12	0.022	±20%	100V,	-
Q503		transistor	2SC634	C507	1-105-877-12	0.022	±20%		-
Q504		transistor	2SA611	C508	1-105-877-12	0.022	±20%		
				C509	1-105-877-12	0.022		100V,	
PTH1	1-800-064	posistor	SB-26	C510	1-105-877-12			100V,	-
PTH 2	1-800-064	posistor	SB-26	C511	1-121-800	4,700	±100%		electrolytic
				C512	1-121-800	4,700	±100%		electrolytic
				C513	1-121-234	470	±100%		electrolytic
			C515	1-121-384	100	±100%		electrolytic	
	TRAN	SFORMER		C516	1-121-384	100	±100%		electrolytic
	1-441-564-14	transformer,	power	C517	1-121-384	100	±100%		electrolytic
				C518	1-121-384	100	±100%		electrolytic
				1					-

CAPACITORS

All capacitance values are in μF except as indicated with p, which means $\mu \mu F$.

C101(C201) 1-121-343 1 $\pm ^{150}_{10}\%$ 50V, electrolytic C102(C202) 1-105-821-12 0.001 $\pm 20\%$ 50V, mylar

RESISTORS

All resistance values are in Ω , $\pm 5\%$, $\frac{1}{4}W$ and carbon type unless otherwise indicated.

R101(R201) 1-242-713 47 k R102(R202) 1-242-745 1 M

TA-1144

Ref. No.	Part No.	Description	Ref. No.	Part No.	Description
R103(R203)	1-242-681	2.2 k	R169(R269)	1-242-689	4.7 k
R105(R205)		470	R170(R270)		3.9 k
R106(R206)		470 k	,		
R107(R 207)		180	R301(R401)	1-244-745	1 M
R108(R208)	1-242-665	470	R302(R402)	1-244-723	120 k
R109(R209)		5.6 k	R304(R404)		1.5 k
R110(R210)		1.2 M	R305(R405)	1-244-647	82
R111(R211)	1-242-661	330	R306(R406)	1-244-706	24 k
R112(R212)	1-242-713	47 k	R307(R407)	1-221-967	10 k (B) ±20%, semi-fixed
R113(R213)	1-242-719	82 k	R308(R408)	1-244-681	2.2 k
R114(R214)	1-242-689	4.7 k	R309(R409)	1-244-693	6.8 k
R121(R221)	1-244-697	10 k	R310(R410)	1-221-967	10 k (B) $\pm 20\%$, semi-fixed
R122(R222)	1-244-719	82 k	R313(R413)	1-244-691	5.6 k
R123(R223)	1-244-735	390 k	R314(R414)	1-244-663	390
R124(R224)	1-222-273	250 k, variable	R315(R415)	1-202-557	220
R125(R225)	1-222-274	250 k, variable	R316(R416)	1-244-625	10
R126(R226)	1-242-701	15 k	R317(R417)	1-244-625	10
R127(R227)		68 k	R318(R418)	1-244-649	100
R131(R231)	1-242-737	470 k	R319(R419)	1-244-673	1 k
R132(R232)	1-242-663	390	R320(R420)	1-244-673	1 k
R133(R233)		15 k	R321(R421)		$0.5 \pm 10\% \ 1.5W$, wire-wound
R134(R234)		390 k	R322(R422)		$0.5 \pm 10\% \ 1.5$ W, wire-wound
R135(R235)		470	R323(R423)		10 $\pm 10\%$ ½W, composition
R136(R236)		470	R324(R424)		470
R137(R237)		5.6 k	R325(R425)		470 ±10% ½W, composition
R138(R238)		1.2 k	R326(R426)		1.5 k
R139(R239)	1-242-735	390 k			
R140(R240)	1-242-709	33 k	R501	1-242-719	82 k
R141(R241)	1-242-669	680	R502	1-242-667	560
R142(R242)	1-242-655	180	R503	1-242-719	82 k
R143(R243)	1-242-695	8.2 k	R504	1-242-659	270
R144(R244)	1-242-701	15 k	R505	1-242-697	10 k
R145(R245)	1-242-719	82 k	R506	1-244-705	22 k
R146(R246)	1-242-691	5.6 k	R507	1-244-705	22 k
R151(R251)	1-242-657	220	R508	1-244-649	100
R152(R252)	1-242-659	270	R509	1-244-649	100
R153(R253)	1-242-665	470	R510	1-242-659	270
R154(R254)	1-242-671	820	R511	1-202-581	2.2 k
R155(R255)	1-242-685	3.3 k	R512	1-244-697	10 k
R156(R256)	1-242-705	22 k	R513	1-244-681	2.2 k
R157(R257)	1-242-703	18 k	R514	1-244-689	4.7 k
R158(R258)	1-242-693	6,8 k			
R159(R259)	1-242-685	3.3 k			
R160(R260)	1-242-681	2.2 k			
R161(R261)	1-242-687	3.9 k		SW	ITCHES
R162(R262)	1-242-689	4.7 k	S1	1-514-601	switch, rotary (FUNCTION 1)
R163(R263)	1-242-689	4.7 k	S2	1-514-600	switch, rotary (FUNCTION 2)
R164(R264)	1-242-691	5.6 k	S3	1-514-598	switch, slide (MONITOR)
R165(R265)	1-242-693	6.8 k	S4	1-514-508	switch, rotary (MODE)
R166(R266)	1-242-693	6.8 k	S5 }		(LOUDNESS)
R167(R267	1-242-691	5.6 k	S13 }	1-514-604	switch, push (REMOTE SPEAKER)
R168(R268	1-242-689	4.7 k	·S14)		(MAIN SPEAKER)



	Ref. No.	Part No.	Description	Ref. No.	Part No.	Description
	S6	1-514-637	switch, slide (TONE TREBLE, LEFT)		1-507-163	phono jack, 4-p
	S7	1-514-637	switch, slide (TONE TREBLE, RIGHT)		1-507-265	jack, headphone
	S8	1-514-637	switch, slide (TONE BASS, LEFT)		1-509-029	DIN connector
	S9 -	1-514-637	switch, slide (TONE BASS, RIGHT)		1-509-341	AC outlet
	S10)		(LOW FILTER)		1-517-021	socket, pilot lamp
	S11 >	1-514-602	switch, push (HIGH FILTER)		1-518-052	lamp, pilot
	(S3)		(MONITOR)		1-526-165	voltage changeover block
	S12	1-514-524	switch, slide (PRE AMP/POWER AMP)			(General Export Model only)
	S15	1-514-599-12	switch, seesaw (POWER)		1-532-214	fuse (USA, CANADA Model)
		{	(General Export Model)		1-532-255	fuse (General Export Model)
		1-514-599-22	switch, seesaw (POWER)		1-534-487	cord, power (General Export Model)
			(USA, CANADA Model)		1-534-526	cord, power (USA, CANADA Model)
					1-536-151	terminal strip, 2L2
						(USA, CANADA Model only)
					1-536-179	terminal strip, 1L1 (C)
					1-536-182	terminal strip, 2L2 (C)
MISCELLANEOUS				1-536-183	terminal strip, 2L3 (C)	
		1-231-057-12	encapsulated component, $0.033\mu\text{F} + 120\Omega$		1-536-189	terminal strip, 1L1 (B)
		1-507-162	phono jack, 10-p		1-536-226	terminal strip, 4-p